RTx Controller Board Design Document

RocketTracks Capstone 2014

The RocketTracks Controller board controls the position of the axes on the RocketTracks camera and antenna pointer. The RTx Controller Board features an Ethernet port for communication with input control devices, as well as a USB port to aid in firmware development and debugging. Commands and tracking data will be sent via Ethernet to the RTx Controller board, and the onboard microcontroller will process the data and output PWM and other control signals to the Generic Motor Driver boards for each axis.



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# Axis Position Feedback

## Axis Position Feedback Overview

RocketTracks uses a potentiometer as a position sensor for each axis. The output voltage is filtered and compared to the input reference voltage via an on-board ADC. The Low-Pass Filter is designed based on control theory requirements, and is a compromise of noise-reduction and phase margin requirements.

## Analog-to-Digital Converters (ADCs) for Feedback circuits

### Component List

#### ADC1

|  |  |  |  |
| --- | --- | --- | --- |
| C1 | C4 | C5 | ADC1 |

#### ADC2

|  |  |  |  |
| --- | --- | --- | --- |
| C2 | C6 | C7 | ADC2 |

#### ADC3

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
| C3 | C8 | C9 | R16 | ADC3 |

#### ADC4

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
| C40 | C41 | C42 | R20 | ADC4 |

#### Analog Reference Voltage Regulator

|  |  |  |  |
| --- | --- | --- | --- |
| C23 | C24 | C25 | REF1 |

### Design Overview

#### ADC Resolution

The resolution of the axis position feedback ADC’s corresponds to the resolution of measurement of the angular position of the axis. Assuming the potentiometer provides a resistance through the axis range of motion which is linear with angle and corresponds to a full-range output voltage sweep through a 360-degree rotation, we have:

The tracking precision required at full-range is then:

We must track a ~2m length object at distances in excess of 18,000ft. However, we need not stay perfectly centered on the rocket at this distance, as video will not be at full zoom, and telemetry signals require less precision than video. Assuming we want to keep the rocket both in the frame and zoom such that the rocket length is 5% of the frame, the tracking resolution at this range becomes:

However, the control system will not be capable of tracking to 1 LSb of the ADC, so as a rule of thumb we will assume tracking precision to within 30% of ADC resolution. Then we have:

As ADC’s are most commonly available in power-of-2 resolutions, a 16 bit ADC will be used.

#### ADC Digital Interface

Given a sample rate of 2000Hz as described in section B.3.a below, we must have a data bandwidth of 2kSamples/sec, with a sample size of 16 bits or 2 Bytes. We must then have a data bandwidth of 4kB/s for each ADC, or 16kB/s if they are on a shared or daisy-chained bus. However, latency is of great concern in a control system, so it is not sufficient that the data transfer complete within the sample period.

A daisy-chain SPI interface allows a single sample command to be issued to all ADC’s simultaneously, and allows a single data transfer from all axes to be performed with lower overhead as compared to a chip-select based SPI interface.

#### ADC and Analog Reference Voltage Regulator Choice

Common ADC data buses are I2C and SPI. The AD7685 is a 16-bit ADC supporting both SPI and daisy-chain serial interfaces at up to 55MHz, or more than 6.5MB/s. It also has a sample rate of up to 250kSamples/s, and a sample-to-data ready time of no more than 2.2us, minimizing latency and satisfying throughput requirements.

##### ADC Supply Voltages

The AD7685 has separate supplies for the converter and for the digital I/O interface. was chosen to match that of the microcontroller, while selection was based on the desire to minimize conversion latency, as higher voltages allow for faster conversion times as well as higher conversion rates. The following voltages were chosen:

##### Reference Voltage Regulator Choice

A stable and noise-free reference voltage is required for the ADC and feedback position sensor potentiometer circuits. The chosen analog reference voltage regulator is recommended for use with the AD7685, and is offered in a range from   
 The model, ADR435, was chosen as the higher voltage maximizes the signal-to-noise ratio.

##### ADC Decoupling Capacitors

Per the datasheet, 0.1uF capacitors were chosen to decouple the supply pins. A 1206-package 22uF capacitor with an X5R temperature coefficient decouples the analog reference input pin, as this is the recommended value when using an ADR43x reference voltage regulator.

##### Analog Reference Supply Decoupling Capacitors

The ARef regulator’s supply pin is decoupled with a 10uF and 0.1uF capacitor, and the output is decoupled with a 0.1uF capacitor, per the device datasheet.

### Summary of Parameters

## Low-Pass Filters for Feedback ADCs

### Component List

#### ADC1 Feedback LPF

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| R1 | R2 | R3 | C10 | C11 | C12 | C13 | OPAMP1-A |

#### ADC2 Feedback LPF

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| R4 | R5 | R6 | C14 | C15 | C16 | C17 | OPAMP1-B |

#### ADC3 Feedback LPF

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| R7 | R8 | R9 | C18 | C19 | C20 | C21 | OPAMP2-A |

#### ADC4 Feedback LPF

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| R17 | R18 | R19 | C36 | C37 | C38 | C39 | OPAMP2-B |

### Design Overview/Component Choice

#### Control Bandwidth and Cutoff Frequency

The control bandwidth frequency for the closed-loop control system was chosen based on the requirement to track fast-moving objects with video during manual and automated control operation. The cutoff frequency for the ADC input LPF is specified to be one decade higher than . This convention places far enough above the to prevent the LPF from limiting performance at the , while still providing satisfactory noise filtering.

#### ADC 1-bit Frequency, desired noise level and Filter Order

The frequency of the ADC’s LSB is the minimum frequency at which we will observe a change on the least significant bit. The maximum noise level desired at is -96dβ. must be a low enough frequency such that the Nyquist rate is reasonable given our choice of ADC’s and microcontroller. With a 3rd Order LPF with our , we have:

The Nyquist rate, or minimum rate we must sample the ADC’s is then , which is a reasonable sample rate for the system.

#### Topology

A Sallen-Key topology Butterworth Low-Pass Filter was chosen due to its simplicity, and the ability to attain 3rd-order filtering and a low with relatively low RLC values in combination.

#### Op-Amp

The AD861x Op-Amp was chosen to produce the Sallen-Key topology because it is recommended for use in conjunction with the chosen ADC’s.

### Consequences

#### Control Rate and ADC Sampling

A rule of thumb for minimum control rate is , then:

The Nyquist rate must also be satisfied, so the sample rate must be:

Choosing and gives us 20 samples per control loop iteration.

### Summary of Parameters

# Microcontroller

# Ethernet Port

## Ethernet Overview

RocketTracks uses the Ethernet protocol to receive command and tracking data to be used by the microcontroller for processing. The microcontroller has an onboard 10/100 Ethernet MAC which is interfaced to an external Ethernet PHY. The Ethernet PHY has a connector with built in magnetics for proper signal integrity. An additional power over Ethernet (PoE) controller maintains appropriate power levels to be supplied over the Ethernet interface.

## Ethernet PHY

### Component List

|  |  |  |  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| IC2 | JP1 | R23 | R24 | R26 | R27 | R30 | R31 | R33 | R34 | R35 |
| C52 | C53 | C56 | C57 | C58 | C59 | C60 | C61 | C62 | C63 | C64 |
| C65 | C66 | C67 | C68 | C69 | C70 | C71 |

### Design Overview

Texas Instrument’s TLK110 was chosen as the Ethernet transceiver for its versatile modes of operation and use of supply voltage which was already present and needed on the RTx controller by other components (eliminating the need for additional voltage regulators). The component operates from a single 3.3VDC power supply.

The transceiver is capable of operating in Media Independent Interface (MII) and Reduced Media Independent Interface (RMII) modes. Although the RMII mode utilizes fewer pins on the transceiver and therefore requires fewer GPIO pins from the microcontroller, with the chosen microcontroller there is no need to limit the number of GPIO pins used for the design. In addition, MII mode operates at a data rate that is half that of RMII which reduces the impact on EMC emissions. The MII interface is also the recommended mode for use in real-time applications, which is critical for video tracking.

The surplus of capacitors are all recommendations by the manufacturer to ensure proper data transmission and reception. Numerous bypass capacitors are placed close to the device itself to ensure proper supply voltage levels during operation and signal integrity.

The Ethernet transceiver also requires a clocked input either from a separate external oscillator or from a clock signal coming from the microcontroller. Since the microcontroller has the ability to provide a clock signal to the transceiver, adding a separate crystal oscillator seemed redundant. There are also sufficient GPIO pins to support this. Therefore the microcontroller will supply the Ethernet transceiver with its clock input.

### Summary of Parameters

The MII interface is used to ensure no latency occurs while communicating with external devices.

A 25MHz clock signal is required from the microcontroller to synchronize timing of data transmission and processing. This will be sourced from the microcontroller.

Although the JTAG scheme is present on the device, it was not seen why it would be necessary for the purposes of this project. Therefore, instead of creating pin designations to incorporate this functionality, each of the JTAG interface pins have been connected to headers for available future use.

## Ethernet Connector

### Component List

|  |  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- | --- |
| X8 | R25 | R28 | R29 | R32 | C44 | C48 | C50 | C51 |

### Design Overview/Component Choice

The Ethernet protocol requires signal isolation through transformer coupling. This can be achieved from a dedicated LAN Discrete Transformer Module or from an Ethernet connector with incorporated transformers. A connector with incorporated transformers was chosen to reduce needed board space and improve signal reliability. The connector transformers also support center-tapping, which is used on the controller board to supply PoE. Built in LEDs allow for visual Ethernet diagnosis at the connector itself.

## Power over Ethernet (PoE)

### Component List

|  |  |  |  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| IC1 | F1 | LED1 | L1 | C43 | C47 | C49 | D1 | D2 | R\_LED1 | POE |

### Design Overview

Linear Techonology’s LTC4263 was chosen in order to incorporate PoE to the RTx design. The component is a single PSE controller compliant with IEEE 802.3af standard. Although other models would allow for PoE+, which would offer greater output power tolerance, the 15W provided by this controller is sufficient to source power to the external devices requiring power from Ethernet.

The PoE controller circuit was taken directly from the product datasheet when used from a single 48VDC supply and incorporated with indicator LED for diagnostic purposes.

# USB Development/Debug Port

## Component List

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
| R21 | R22 | C45 | C46 | U2 | X4 |

## Design Overview/Component Choice

The USB port requires ESD protection. For this TI’s TPD4S012 was chosen because it was a cheap and straightforward solution. A 22Ω current-limiting resistor was placed in series on the D+ and D- line. The two capacitors were placed to reduce noise.

# Supply Voltage Regulation/Filtering

# Motor Driver Outputs